

Treatment of Vegetable Oil Refinery Wastewater Using Response Surface Methodology

Mohammed CH^{1*}, Hajar BA¹, Salah S¹ and Abdelrani A²

¹Hassan II University, Morocco

²Cadi Ayyad University Marrakech, Morocco.

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ABSTRACT

Nowadays, wastewater from vegetable oil refining (VORW) heavily loaded with fats, oils, phenol, etc. presents serious problems for the environment. Indeed, in order to minimize the impacts on the receiving environment (surface water, groundwater, etc.), the treatment of these discharges becomes mandatory. Currently, several techniques are widely used to control the pollution from these discharges. The present work aims to study the efficiency of the flocculation-coagulation process using Ferric chloride (FeCl₃) as a coagulant coupled with a cationic polymer (polyacrylamide) as a flocculant for the treatment of these wastes. The surface methodology response (RSM) was used to study the effects of the main factors that influence the process and their interactions. The optimal conditions obtained during the study were 1.3g /L of coagulant (FeCl₃) and 8.6 mg / L of flocculant at pH round 6.4. The results obtained while respecting the optimal conditions showed a reduction of 90% of COD (Chemical oxygen demand) and 95% of turbidity and oils and fats. The analysis of variance showed a high coefficient of variance (R) values of 0.91 for COD and 0.80 for turbidity, oil, and grease removal, respectively. Thus, ensuring an adjustment satisfactory second-order regression model with experimental data. Using the experimental design, this statistical methodology allows achieving optimal conditions very close to the experimental ones. It constitutes a suitable approach for optimizing the coagulation-flocculation process by experiment confirmation. Thus, the coagulation method developed in the present work can be considered useful for the pretreatment process of vegetable oil refinery wastewater prior to biological treatment.

Keywords: Oil, Refinery, Wastewater, Treatment, Optimization

INTRODUCTION

The industrial units of vegetable oil refineries are large consumers of water and, therefore large producers of wastewater heavily loaded with pollutants [1]. These wastewaters have high chemical oxygen demand (COD), oil & grease (O&G) levels, along with elevated dissolved solid concentrations [2,3]. Furthermore, their transport presents a high risk of clogging in pumps and piping. The waste streams that come out of vegetable oil refineries create serious environmental problems such as a significant threat to aquatic life due to its high organic content [4]. For these reasons, vegetable oil refinery wastewater (VORW) cannot be treated in a conventional municipal wastewater treatment plant. Hence, its treatment is crucial before the disposal step. This has driven many researchers towards developing suitable treatment technologies by using oil in water mixture to produce treated water of appropriate quality for reuse and recycling [5,6].

The characteristics of wastewater depend mainly on the type of oil processed as well as on the process applied. Different processes have been described in the literature for the

treatment of wastewaters with high oil and grease content. In fact, the commonly used are chemical destabilization [3], membrane processes [7,8] and electrochemical methods [1]. The process of flotation for treating oily wastewaters was also already examined [9,10]. Chemical unit processes have been found to be also cost-effective, easy to handle and can be considered as an alternative treatment for energy saving. This process may be used as a pre-treatment step prior to biological treatment to improve the biodegradability of the wastewater during the biological treatment. The iron (III) chloride hexahydrate, FeCl₃·6H₂O, is a widely used

Corresponding author: Mohammed CH, Hassan II University, Morocco, Tel: +212 666 900660; E-mail: mohammed.chatoui@gmail.com

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coagulant. It has been widely used to treat oily wastewater [11,12]. Many factors can affect the efficiency of chemical treatment including the type and dosage of coagulant/flocculant [13], pH [14], mixing speed and time [15], temperature and retention time [16], etc. Due to the complexity of the optimization process, it would be better and less consuming to find the optimum value with highest efficiency by gathering all these factors. Since then, many experiments should be realized to reach this optimum: one factor is varied while all the others are kept fixed from one test to another at specific conditions. This optimization is usually time consuming concerning the exact value of the optimum due to the interactions between the varied factors that are ignored. In order to have a better optimization, experimental design and Response Surface Methodology (RSM) have been proposed to define the influence of individual factors, their interactions, and the isoresponses curves for each response. RSM is an efficient tool for Process Optimization; it's a multivariate statistical technique used to optimize processes. With RSM, a limited number of experiments are enough to determine which factors are influencing the process's most efficiently. There are different fields where RSM gets used, including the preparation of activated carbons from Argan shells [17], the preparation of chitosan from beet molasses, and the synthesis of N-carboxy butyl chitosan [18]. Therefore, for optimizing specific processes in the food industry, pharmaceuticals industry, material manufacturing, biotechnology [19-21], and environmental science [22], this method has been widely approved and efficient. In this context, the aim of this work is to optimize the coagulation-flocculation process for the wastewater treatment of a Moroccan agro-industrial company. In the first stage, a Central Composite Design (CCD) was used to study the effect and first-order interactions of various factors (coagulant dosage, flocculant dosage and pH) on the coagulation-flocculation process, and, in the second stage, those factors are optimized using RSM and multicriteria optimization with the desirability function.

MATERIALS AND METHODS

Wastewater samples

The wastewater samples used in this study were obtained from the discharge of a Vegetable Oil Refinery located in Casablanca (Morocco). Upon collecting the samples, their physicochemical characteristics were investigated to measure their level of pollution and to select the appropriate treatment. The samples were collected in glass bottles and kept in a refrigerator during experimentation. Chemical characterizations were performed by defining the following parameters: the aqueous phase pH, the temperature, the turbidity, the oil and grease amount, and the chemical oxygen demand (COD). The turbidity was determined by using turbidity meter (HI 93703 Microprocessor turbidity meter). The concentration of emulsified oil was determined by the extraction colorimetric technique. Hexane was used

as a solvent to extract the oil from the oil in water emulsion [23]. The COD was determined using Open Reflux Method (5220-B). Most types of organic matter are oxidized by a boiling mixture of chromic and sulfuric acids. A sample is refluxed in a strongly acid solution with a known excess potassium dichromate ($K_2Cr_2O_7$). After digestion, the remaining unreduced $K_2Cr_2O_7$ is titrated with ferrous ammonium sulfate to determine the amount of $K_2Cr_2O_7$ consumed, and the oxidizable matter is calculated in terms of oxygen equivalent the 2-hour time is adopted for the oxidation of organic matter under standard conditions. Some samples with very low COD or with highly heterogeneous solids content may need to be analyzed in replicate to yield the most reliable data. Mohr's salt determined the excess dichromate $K_2Cr_2O_7$. Other physicochemical parameters (BOD, TSS....) for wastewater characterization measurement were performed according to standard methods [24].

Coagulation-flocculation experiments

The coagulation-flocculation experiments were carried out using the jar test method in 500 mL beakers. After the coagulant was added with a varying dosage from 582 to 1872 mg/L, the solution pH was adjusted to 4.32 and 7.68 by adding 0.1 M hydrochloric acid or 0.1 M sodium hydroxide solutions. The sample was directly agitated at a constant speed of 200 rpm for 2 min. Then, the flocculant was added with a dosage varying from 1.04 to 11.96 mg/L followed by a slow stirring at 40 rpm for 40 min; thereafter, a settlement for 60 min was performed. After that, samples were taken from the water level around 2 cm underneath the surface to measure the physicochemical parameters of the supernatant.

Experimental design and data analysis

The central composite design (CCD), with five replicates at the central points, was employed to fit a second-order polynomial model and obtain the experimental error. The CCD was applied with three design factors and five levels. The factors are the pH (X_1), the flocculant dosage (X_2) and the coagulant dosage (X_3). The coded levels and the natural values of the factors set in this statistical experiment are shown in **Table 1**. The central values chosen for the experimental design were as follows: Coagulant dosage, 1200 mg/L; flocculant dosage, 6.5mg/L; and pH 6. The value of α for rotatability depends on the number of points in the factorial portion of the design, which is given in **Equation (1)**:

$$(N_F) \quad (1)$$

Where N_F is the number of points in the cube portion of the design ($N_F = 2^k$, k is the number of factors). Since, there are three factors, the N_F number is equal to $2^3 (=8)$ points, while α is equal to $(8)^{1/4} (=1.682)$ according to **Equation (1)**. (**Table 1**)

Table 1. Factors and levels used in the 2³ central composite designs for coagulation/flocculation process.

Unidimensional variables	Factors		Levels of factors				
			-α	-1	0	1	+α
X ₁	pH		4.32	5	6	7	7.68
X ₂	Flocculant dosage	mg/L	1.04	3.25	6.5	9.75	11.96
X ₃	Coagulant dosage	mg/L	528	800	1200	1600	1872

COD, Turbidity and Oil & Grease removal percentage were selected as the dependent variables. The response variable was fitted by a second-order model in the form of quadratic polynomial equation (2):

$$\sum_{i=1}^3 b_i X_i + \sum_{i=1}^3 b_{ii} X_i^2 + \sum_{i < j} b_{ij} X_i X_j \quad (2)$$

Y is the response variable to be modeled; X_i, and X_j the independent variables that influence Y; b₀ is the constant term, b_i represent the coefficients of the linear parameters (principal effect), b_{ij} the ijth interaction coefficient and b_{ii} the quadratic coefficient. The actual design used in this work is presented in **Table 2**.

Table 2. The Central Composite Experimental Design, experimental conditions and responses Y: COD, Turbidity and Oil & Grease removal.

N° Exp	Design of experiments			Operating conditions			Experimental Response (%)		
	X ₁	X ₂	X ₃	pH	Flocculant dosage mg/L	Coagulant dosage mg/L	Y ₁ COD removal	Y ₂ Turbidity removal	Y ₃ O & G removal
1	-1.00	-1.00	-1.00	5.00	3.25	800	71.7	85.7	74.7
2	1.00	-1.00	-1.00	7.00	3.25	800	79.7	87.7	76.7
3	-1.00	1.00	-1.00	5.00	9.75	800	73.7	84.7	80.7
4	1.00	1.00	-1.00	7.00	9.75	800	81.6	91.0	86.3
5	-1.00	-1.00	1.00	5.00	3.25	1600	67.7	74.7	71.3
6	1.00	-1.00	1.00	7.00	3.25	1600	79.8	88.3	76.7
7	-1.00	1.00	1.00	5.00	9.75	1600	77.8	89.0	78.7
8	1.00	1.00	1.00	7.00	9.75	1600	81.8	88.3	85.7
9	-1.68	0.00	0.00	4.32	6.5	1200	75.8	88.3	82.0
10	1.68	0.00	0.00	7.68	6.5	1200	83.8	89.0	90.0
11	0.00	-1.68	0.00	6.00	1.04	1200	79.9	82.0	86.0
12	0.00	1.68	0.00	6.00	11.96	1200	89.9	95.7	91.3
13	0.00	0.00	-1.68	6.00	6.5	528	71.4	84.3	76.7
14	0.00	0.00	1.68	6.00	6.5	1872	79.7	91.7	91.0
15	0.00	0.00	0.00	6.00	6.5	1200	88.1	94.3	92.3
16	0.00	0.00	0.00	6.00	6.5	1200	90.0	92.7	93.3
17	0.00	0.00	0.00	6.00	6.5	1200	87.9	93.7	94.3
18	0.00	0.00	0.00	6.00	6.5	1200	88.4	93.3	93.3
19	0.00	0.00	0.00	6.00	6.5	1200	89.0	94.0	94.7
20	0.00	0.00	0.00	6.00	6.5	1200	88.7	94.7	95.3

Analysis of variances (ANOVA) was used to analyze the data to obtain the interaction between the process variables and the responses. The correlation coefficient expressed the quality of the fit polynomial model, and its statistical significance was checked by the F-test. Model terms were selected or rejected based on the P-value (probability) with a 99% confidence level. Three-dimensional plots and their respective contour plots were obtained based on the effects of the levels of two factors. The analysis of the results of each response was achieved by response surface methodology based on a second-order model adequate to predict responses all over the experimental regions. All the calculations (regression, statistical tests, and graphical plots) were performed with NemrodW software [25]. For experimental validation of results, two additional experiments were conducted, in the optimum conditions, to verify the validity of the statistical experimental strategies.

RESULTS AND DISCUSSION

Characterization of VORW

The physicochemical characterization of water samples plays a significant role in understanding the evolution of pollution levels during the time, identifying the nature and concentration of components, and controlling the CF process since the performance of the treatment is highly influenced by the chemical and organic loads. Therefore, two samples were taken each week for three months. Results of physicochemical characterization are summarized in **Table 3**. From obtained results, pH was ranged between 4.22 ± 0.17 and 1.5 ± 0.07 ; it remains acid during the study period, which may be due to the use of sulfuric acid in the deacidification step. The mean values of COD and BOD5 were about 37.7 and 2.9 g/L, respectively, and the COD/BOD5 ratio was around 12, so biological treatment cannot be adopted in this case.

For the turbidity and TSS, the mean values were about 600 NTU and 4594 mg/L, respectively, which indicates that the VORW contains a level of suspended solids responsible for BOD₅ and COD. In the same way, VORW contains a large number of chemical pollutants such as oil & grease (2053 mg/L), phosphorus (556 mg/L), and sulfate (1080 mg/L). The characterization results were consistent with those found by other authors [26-28]. They also found that VORW is highly charged with organic and chemical loads. Generally, the composition of wastewater from the effluent varies widely from day to another day. These fluctuations may be attributed to different types of oils processed and to operating conditions and processes [3]. Wastewater characteristics are not only influenced by the raw materials and the products processed but also by water used in washing procedures during and after production [29]. These factors influenced the observed variation in the COD and BOD₅ values of each wastewater sample in conclusion, the physicochemical analysis revealed that almost all of the parameters indicating that the VORW is highly charged with

organic and chemical pollutants and must be treated further before it can be discharged to any receiving water (**Table 2**).

Table 3. Characterization of vegetable oil refinery wastewater.

Parameters	Average value	Minimum	Maximum
pH	1.5	0.65 ± 0.12	4.22 ± 0.08
Temperature (°C)	33	24 ± 0.05	39 ± 0.01
BOD ₅ at 20°C (mg/L)	2992	1400 ± 4	5800 ± 6
COD (mg/L)	37723	19900 ± 8	61200 ± 14
TSS (mg/L)	4594	1600 ± 0.8	12400 ± 0.6
Oil & grease (mg/L)	2053	400 ± 0.02	6800 ± 0.01
Turbidity (NTU)	600	300 ± 0.01	800 ± 0.01
Dissolved Oxygen (mg/L)	1.13	0.2 ± 0.02	1.6 ± 0.01
Total Kjeldahl Nitrogen (mg/L)	371	123 ± 0.05	684 ± 0.02
Total Phosphorus (mg/L)	556	261 ± 0.08	894 ± 0.1
Sulfate (mg/L)	1080	160 ± 0.62	1960 ± 0.45

Optimization of the coagulation/flocculation process
Statistical analysis

Preliminary experiments were carried out to investigate the effect of the most influencing factors on CF treatment efficiency. The relationship between the three variables (coagulant concentration, flocculent dosage, and pH) and the three important process responses (COD, oil & grease and turbidity removal efficiencies) for the CF process was analyzed using RSM. Further experiments were carried out for the optimization process to obtain a quadratic model consisting of 15 trials with different combinations of the parameters plus five replicates at the center point choosing according to the Box–Behnken design as shown in **Table 2**.

The statistical analysis of the Box–Behnken experimental results, response surface modeling, and optimization of process variables were carried out using NemrodW software (Table 3).

Significant model terms were desired to obtain a good fit in a particular model. The statistical analysis using NemrodW software allowed the development of mathematical equations, where predicted results (Y1, Y2, and Y3 for COD, Turbidity and oil & grease removals, respectively) were assessed as a function of pH (X1), flocculent dosage (X2), and coagulant concentration (X3) and calculated as the sum of a constant, three first-order effects (terms in X1, X2, and X3), three interaction effects (interactive terms in X1X2, X1X3, and X2X3) and three second-order effects (quadratic terms in X12, X22, and X32) according to Equation (2). The results obtained were then analyzed to assess the goodness of fit.

Central composite design (CCD) and fitted regression models as related to the pollutant removal

In the present work, the relationship between tree criteria of the pollutant removal (namely COD, turbidity, and oil & grease) and three controllable factors (namely coagulant concentration, flocculent dosage, and pH) was studied. By applying multiple regression analysis on the design matrix and the responses are given in Tables 4-6, the following second-order polynomial equations in coded form were established to visualize the effects of independent factors on the turbidity, oil & grease and COD removal efficiencies (Equations 3-5).

Table 4. Estimated values of coefficients for response COD removal (Y1).

Coefficient	Standard error	t.exp.	Signification%
b0	88.28	0.53	166.31 < 0.01 ***
b1	3.33	0.35	9.45 0.0457 ***
b2	2.40	0.35	6.82 0.145 **
b3	1.05	0.35	2.99 3.06 *
b11	-3.57	0.34	-10.41 0.0333 ***
b22	-1.77	0.34	-5.15 0.418 **
b33	-5.07	0.34	-14.79 0.0119 ***
b12	-1.03	0.46	-2.23 7.5
b13	0.03	0.46	0.05 95.8
b23	1.03	0.46	2.23 7.5

The experimental response (COD removal) can be described by the model:

$$57(X_1) - 0.77(X_2^2) - 5.07(X_3^2) \tag{3}$$

Table 5. Estimated values of coefficients for response Turbidity removal (Y2).

Coefficient	Standard error	t.exp.	Signification%
b0	93.85	0.29	321.06 < 0.01 ***
b1	1.64	0.19	8.45 0.0671 ***
b2	2.90	0.19	14.97 0.0115 ***
b3	0.27	0.19	1.38 22.6
b11	-2.24	0.19	-11.85 0.0223 ***
b22	-2.17	0.19	-11.48 0.0245 ***
b33	-2.47	0.19	-13.07 0.0167 ***
b12	-1.25	0.25	-4.93 0.493 **
b13	0.57	0.25	2.27 7.2
b23	1.50	0.25	5.92 0.247 **

The model can describe the experimental response (Turbidity removal):

$$57(X_1) - 0.77(X_2^2) - 5.07(X_3^2) - 17(X_1X_2) - 25(X_1X_3) + 50(X_2X_3) \tag{4}$$

Table 6. Estimated values of coefficients for response Oil & Grease removal (Y3).

Coefficient	Standard error	t.exp.	Signification%
b0	94.09	0.45	210.01 < 0.01 ***
b1	2.45	0.30	8.24 0.0732 ***
b2	3.00	0.30	10.08 0.0370 ***
b3	1.32	0.30	4.45 0.731 **
b11	-4.23	0.29	-14.61 0.0123 ***
b22	-3.29	0.29	-11.37 0.0253 ***
b33	-4.99	0.29	-17.23 < 0.01 ***
b12	0.65	0.39	1.67 15.4
b13	0.60	0.39	1.54 18.2
b23	0.10	0.39	0.26 80.1

The model can describe the experimental response (Oil & grease removal):

$$29(X_1) - (X_2) \quad 23(X_3) \quad (5)$$

In Equations. (3), (4), and (5), Y1, Y2 and Y3 correspond to responses of COD, turbidity, and oil & grease removals, respectively; X1, X2, and X3 correspond to independent variables of pH, flocculent dosage, and coagulant concentration, respectively. The positive sign of the coefficient indicates a synergistic effect and the negative sign indicates an antagonistic effect. The model equations and regression coefficients were significant (P < 0.01) and should be included in the model and illustrated that percentage removal of COD, turbidity, and oil & grease were related to all studied factors.

Statistical validation of the model was achieved with the Student's statistical t-test for analysis of variance (NemrodW); it was used to determine the significance of the regression coefficients, and the p value was the indicator of the significance of the test. The more significant t and the smaller value of p, the model, and model terms are more statistically significant [30]. The analysis of variance is essential to test the significance of the model. Therefore, as seen in Tables 4, 5 and 6, the model was tested. We found that the quadratic models were highly significant from the low probability value (< 0.01).

The goodness of fit of the model was checked by determining the correlation between the theoretical and experimental responses (R²). In this case, the R² value for Eq. (3) was 0.91 with a standard deviation of ε = 1.3, for Eq. (4) was 0.80 with a standard deviation of ε = 0.72, and for Eq. (5) was 0.80 with a standard deviation of ε = 1.10. Compared to other studies adopting RSM and Box-Behnken design statistical analysis to optimize industrial wastewater treatment [31,32], our models were considered highly significant. They showed excellent correlations between the experimental results and the predicted values of COD, turbidity, and oil & grease removal from these models.

Surface responses analysis

In order to provide better clarification of the effects of the independent variables and their interactions, two- (2D) and three-dimensional (3D) response surface plots were traced as a function of two factors at a time, carrying the other factor fixed at zero levels. Figure 1 shows the two-dimensional, and three-dimensional response surface plots for the COD removal from VORW treated using the CF process. As showed in the contour plots relating to the COD removal, the result revealed the high interaction between the factors tested; the trough in the response areas/surfaces showed that the optimal conditions for maximal COD removal were precisely inside the design limit. Hence, at fixed pH to 6, maximum COD removal percentages were achieved when coagulant concentration was ranged between 1.2 and 1.23 g/L. In contrast, the flocculent concentration was ranged from 7 to 7.8 mg/L. It was clear from the figures that the

COD removal decreased when the pH of the wastewater was in the neutral field. From Figure 1(b), we can deduce that maximum COD removal was observed when flocculent concentration was fixed equal to 6.5 mg/L under coagulant concentration ranged from 1.1 to 1.3 g/L and pH ranged from 5.9 to 7.2. Contour plots of pH versus flocculent concentration at coagulant concentration fixed to 1.2 g/L presented in Figure 3(a) show that an interaction occurs between flocculent dosage and pH for oil & grease removal as a response; the maximum of oil & grease removal was attained when flocculent concentration ranged from 6.4 to 8.8 mg/L and pH ranged from 5.8 to 7. The following graphical representations, Figure 2 show the behavior of turbidity under the simultaneous change in two variables while fixing the other factor. As can be understood from the elliptical nature of contour plots of turbidity removal, there was a significant interactive effect between the three factors (coagulant concentration, flocculent concentration, and pH). From Figure 2(c), we can conclude that the optimal turbidity removal was observed when the coagulant concentration ranged from 1.2 to 1.4 g/L under flocculent concentration from 6.5 to 7.8 mg/L and pH equal to 6. On the other hand, the contour plots of coagulant concentration versus pH illustrated that the optimal conditions for maximal turbidity removal were achieved when coagulant dosage was ranged from 1.18 to 1.25 g/L and for pH values from 6 to 6.8 (Figure 2(b)). In Figure 2(a), contour plots showed that for coagulant concentration fixed at 1.2 g/L, turbidity decreased with the increase of flocculent concentration independently of pH. The maximum turbidity removal was obtained when pH values were between 6 and 6.8. The CF process efficiency to remove turbidity was highly influenced by the pH values of the treated samples can be concluded. Figure 3 shows the two-dimensional and three-dimensional response surface plots for the oil & grease removal. As showed in the contour plots corresponding to the oil & grease removal, the dome shape revealed the high interaction between the factors tested; the trough in the response areas/surfaces indicated that the optimal conditions for maximal oil & grease removal were inside the design limit. Thus, at fixed pH to 6, maximum COD removal was obtained when coagulant concentration was ranged between 1.1 and 1.3 g/L. In contrast, the flocculent concentration was ranged from 6.4 to 8.8 mg/L. It was clear from the Figure 3(a) that the removal of oil and grease decreased as the pH of the wastewater was in the neutral field. From Figure 3(b), we can deduce that maximum oil & grease removal was observed when flocculent concentration was fixed to 6.5 mg/L under coagulant concentration ranged from 1.1 to 1.3 g/L and pH ranged from 5.5 to 7.1. Contour plots of pH versus flocculent concentration at coagulant concentration fixed to 1.2 g/L presented in Figure 1(a) show that an interaction between flocculent dosage and pH for COD removal as a response; the maximum of COD removal was achieved when flocculent concentration ranged from 7 to 7.4 mg/L and pH ranged from 6.5 to 6.8. The 2D and 3D surface plots

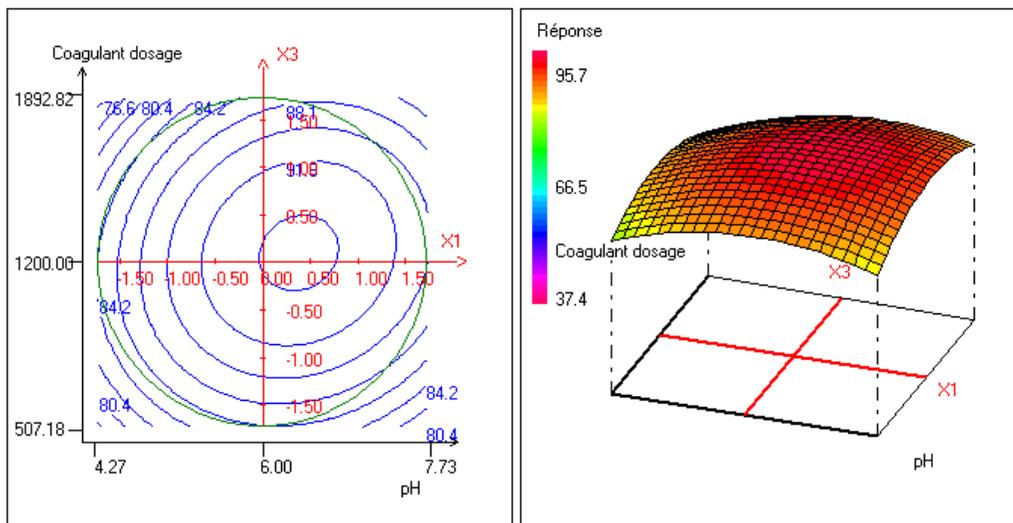
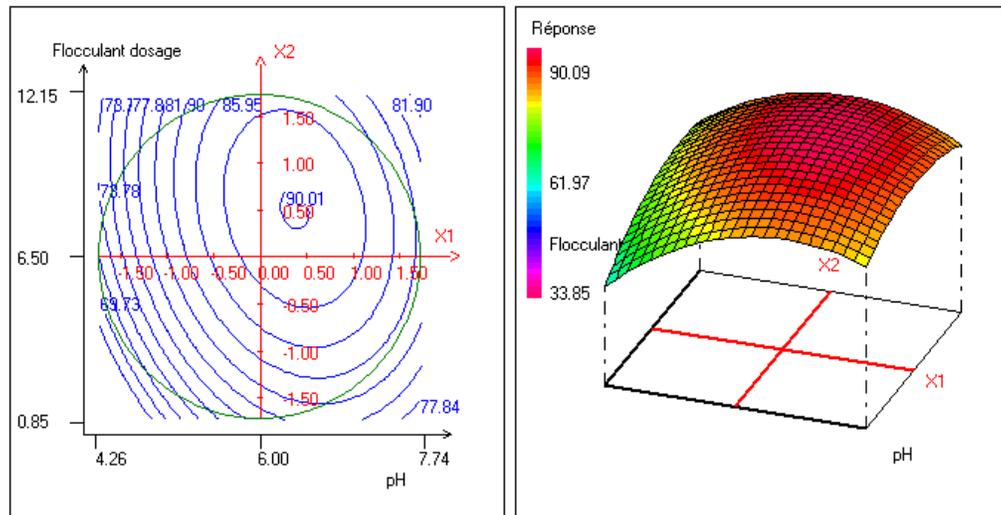
illustrated that the maximum turbidity and COD removals from VORW were obtained under pH six. The concentration of coagulant and flocculent proximate to zero. The optimum experimental conditions for COD, turbidity and oil & grease removals were achieved by solving the equations and by evaluating the response surface contour plots. The optimum values of the tested variables were as follows: coagulant

concentration of 1.26 g/L, the flocculent concentration of 8.6 mg/L, and pH of 6.4, while the maximum of COD, turbidity, and oil & grease removals predicted were around 89.6, 95.3 and 95%, respectively. The models predicted for COD and turbidity removals were confirmed by carrying out the CF experiments at the optimal conditions predicted using RSM.

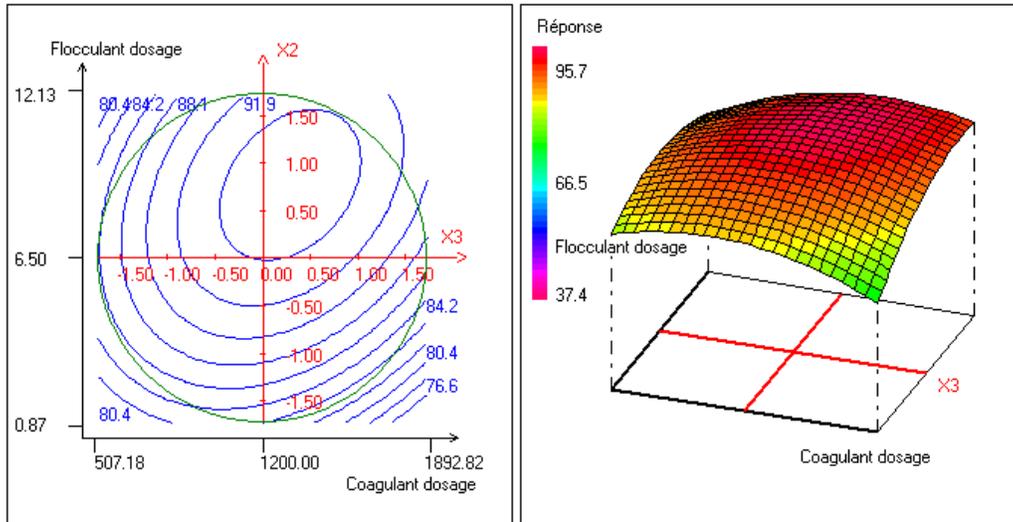
Graphic study in 2D

Graphic study in 3D

(a)



(b)



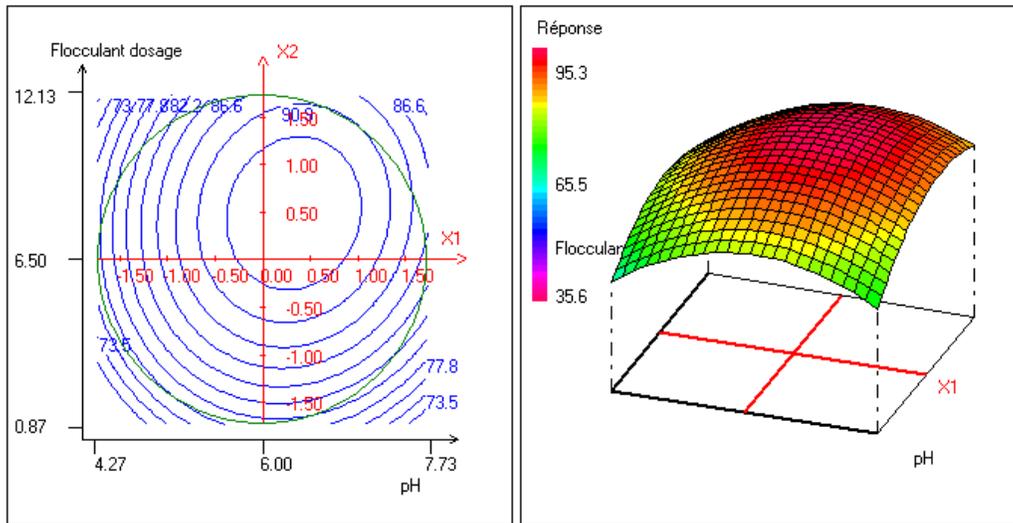
(c)

Figure 1. Variation of the COD removal (%) (iso-response curves) as a function of: a) X_1 (pH) and X_2 (Flocculant dosage), Coagulant dosage = 1200 mg/L; b) X_1 (pH) and X_3 (Coagulant dosage), Flocculant dosage = 6.5 mg/L; c) X_3 (Coagulant dosage) and X_2 (Flocculant dosage), pH = 6.0.

Graphic study in 2D

Graphic study in 3D

(a)



(b)

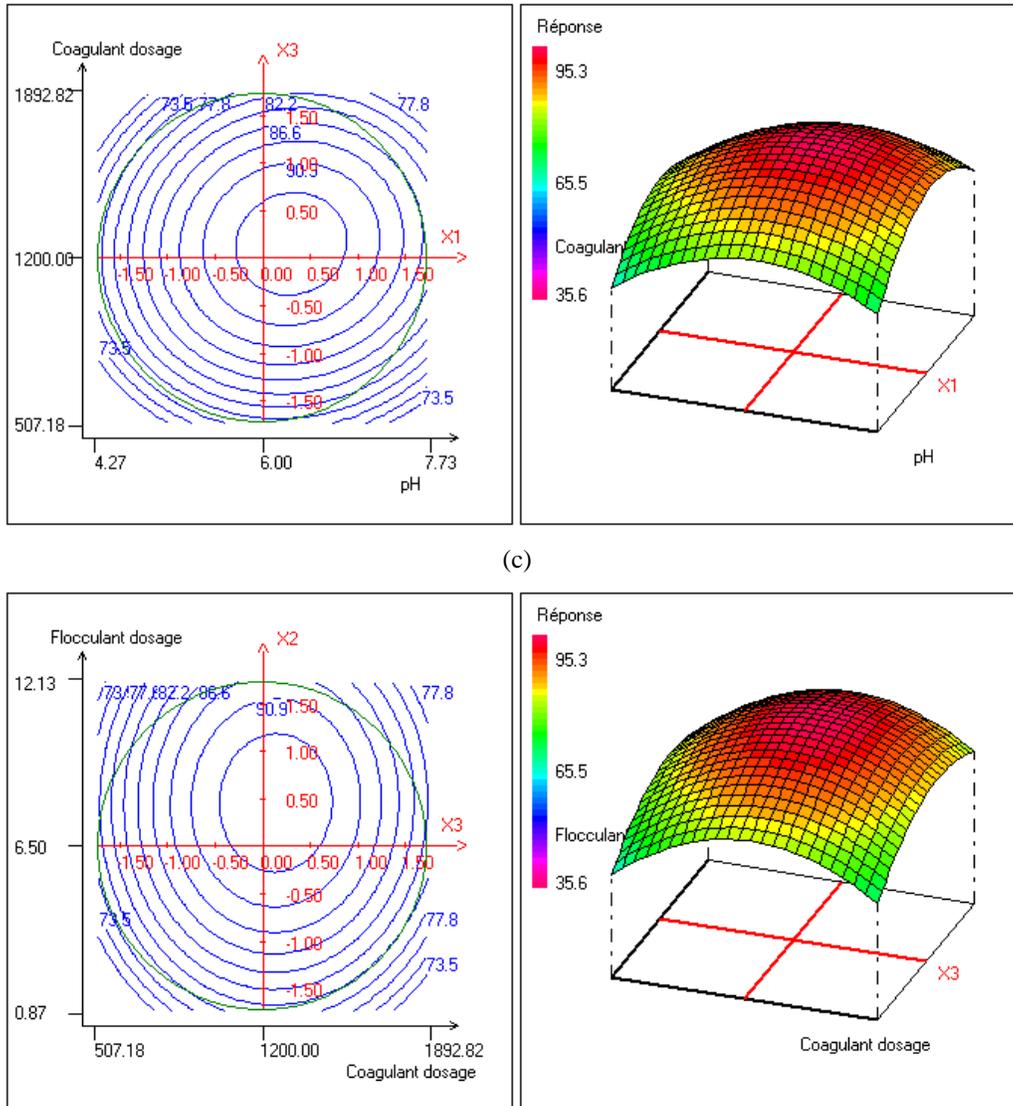
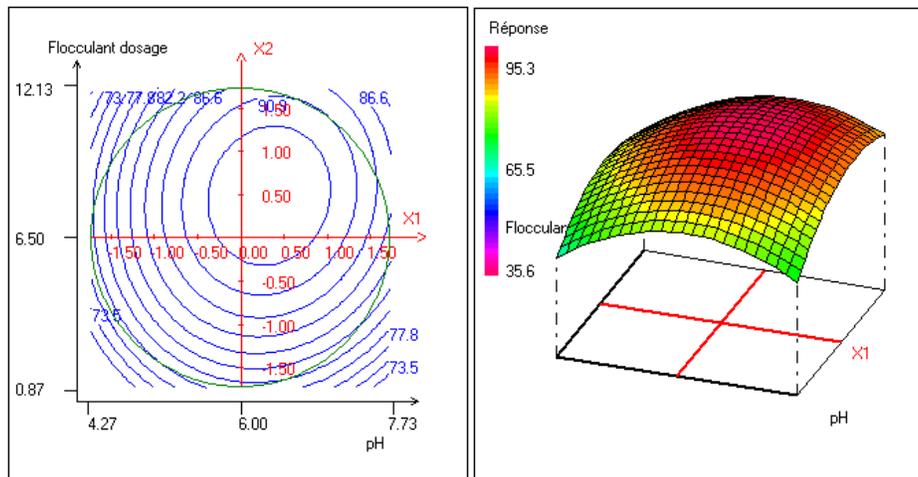


Figure 2. Variation of the Turbidity removal (%) (iso-response curves) as a function of: a) X_1 (pH) and X_2 (Flocculant dosage), Coagulant dosage = 1200 mg/L; b) X_1 (pH) and X_3 (Coagulant dosage), Flocculant dosage = 6.5 mg/L; c) X_3 (Coagulant dosage) and X_2 (Flocculant dosage), pH = 6.0.

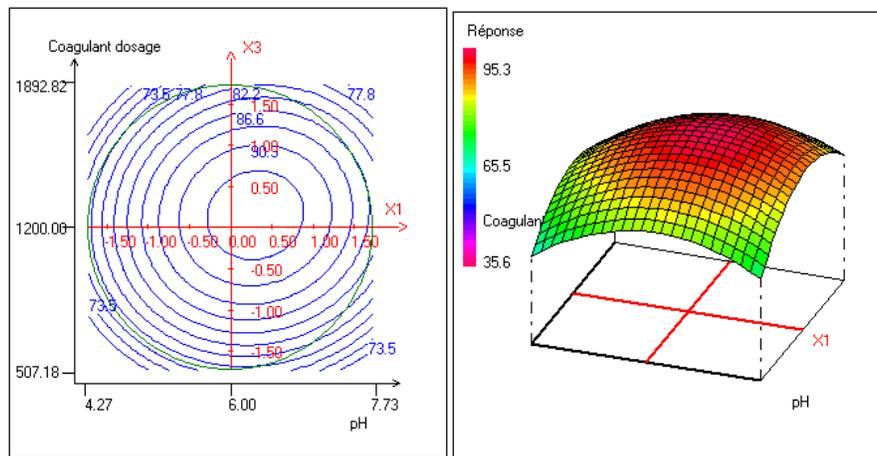
Graphic study in 2D

Graphic study in 3D

(a)



(b)



(c)

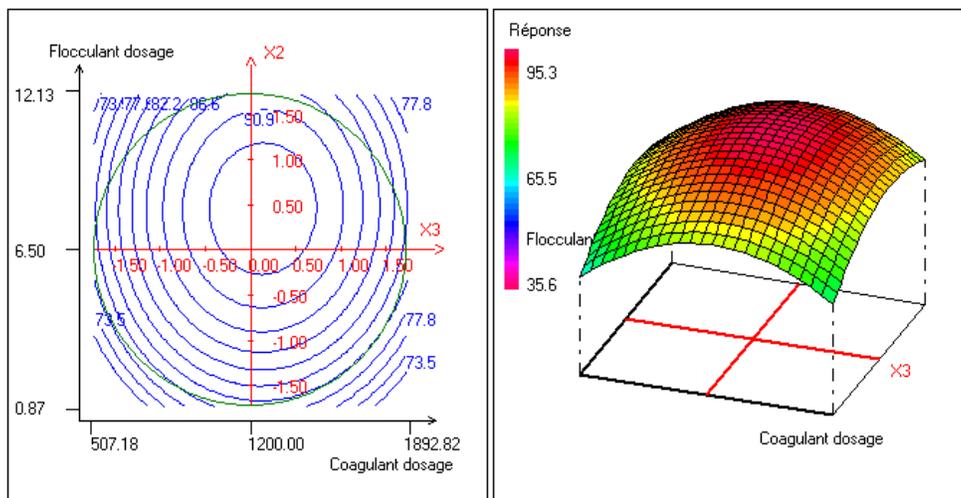


Figure 3. Variation of the Oil & Grease removal (%) (iso-response curves) as a function of: a) X_1 (pH) and X_2 (Flocculant dosage), Coagulant dosage = 1200 mg/L; b) X_1 (pH) and X_2 (Coagulant dosage), Flocculant dosage = 6.5 mg/L; c) X_1 (Coagulant dosage) and X_2 (Flocculant dosage), pH = 6.0.

Desirability function

The desirability function is a method used for defining the best conditions for process adjustment, constructing possible simultaneous optimization of multiple responses. This being so, the best response conditions are attained simultaneously minimizing, maximizing, or seeking nominal values of specifications, depending on the best convenient situation for the process [33].

Each one of the responses ($Y_1, Y_2 \dots Y_k$) of the original set is changed, such that d_i belongs to interval $0 \leq d_i \leq 1$. The d_i value increases when the i th response approaches the imposed limits.

Equation 6 is used to discover the D global index from a combination of each response processed through a geometric mean.

$$(d) \quad (6)$$

The maximum function D provides the best global compromise in the studied area and corresponds to optimal experimental conditions.

Rudimentary desirability functions with the minimum and objective values are illustrated in **Figure 4**, and the low and target value assigned to each objective and the partial desirability's related to the three responses are shown in **Table 7**.

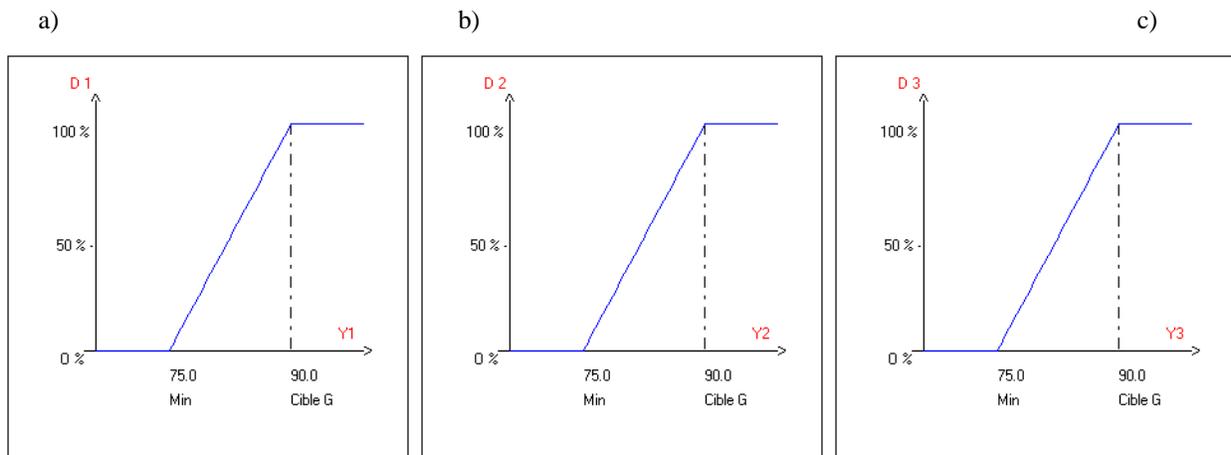


Figure 4. Desirability function. (a) Y_1 (COD removal); (b) Y_2 (Turbidity removal) etc (c) Y_3 (Oil & Grease removal).

Table 7. Low and target value and the partial desirabilities associated to the four responses.

Response	Lower limit	Target value	Weight	d_i %	$d_{i \min}$ %	$d_{i \max}$ %	Y_{Cal} value
Y1: COD removal (%)	75	90	1	97.53	89.02	100.00	89.6
Y2: Turbidity removal (%)	75	90	1	100.00	100.00	100.00	95.0
Y3: Oil & Grease removal (%)	75	90	1	100.00	100.00	100.00	95.3
Desirability				99.17	96.20	100.00	

d_i : partial desirability of response Y_i , $d_{i \min}$: minimal partial desirability of response Y_i , $d_{i \max}$: maximal partial desirability of response Y_i , $Cal. value$: calculated value, $Exp. Value$: experimental value

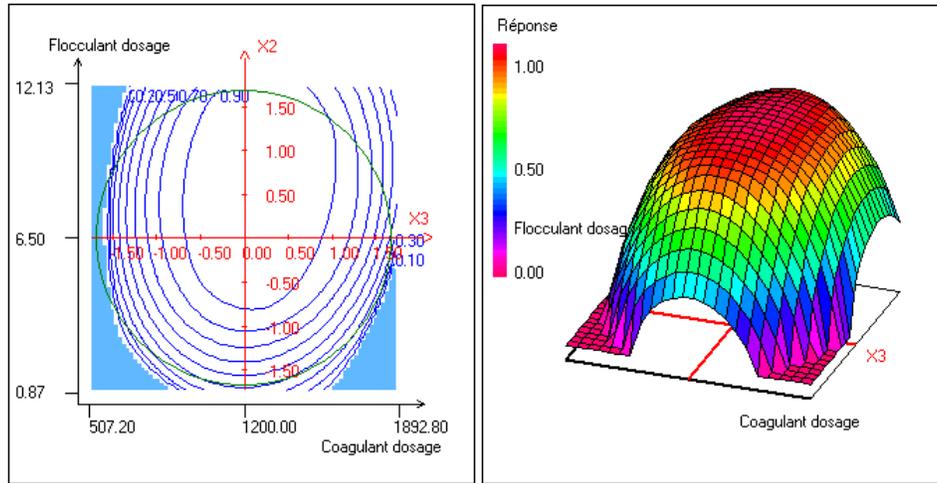
After calculating the NEMROD-W software, the response surface corresponding to global desirability function D is

presented as a contour plot and a three-dimensional plot. The compromise domain is presented in **Figure 5**.

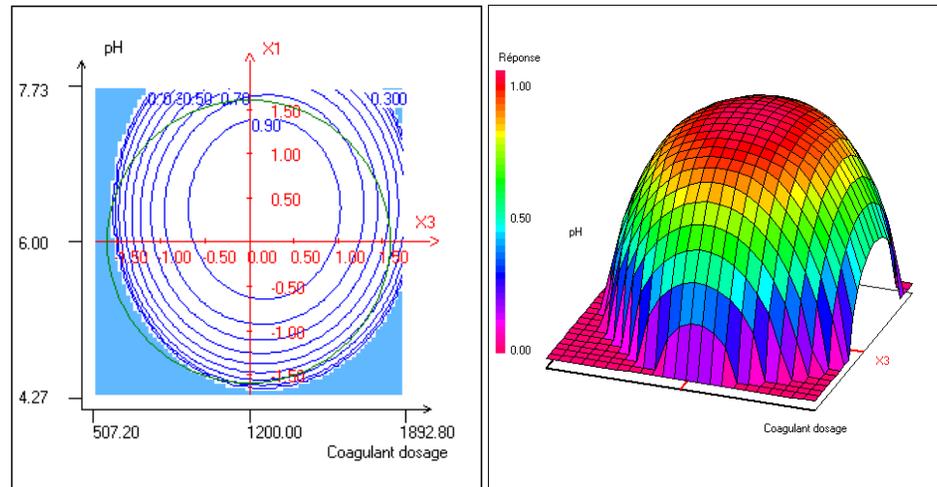
a). Contour plot

b) Three dimensional plot

$$(1)$$



(2)



(3)

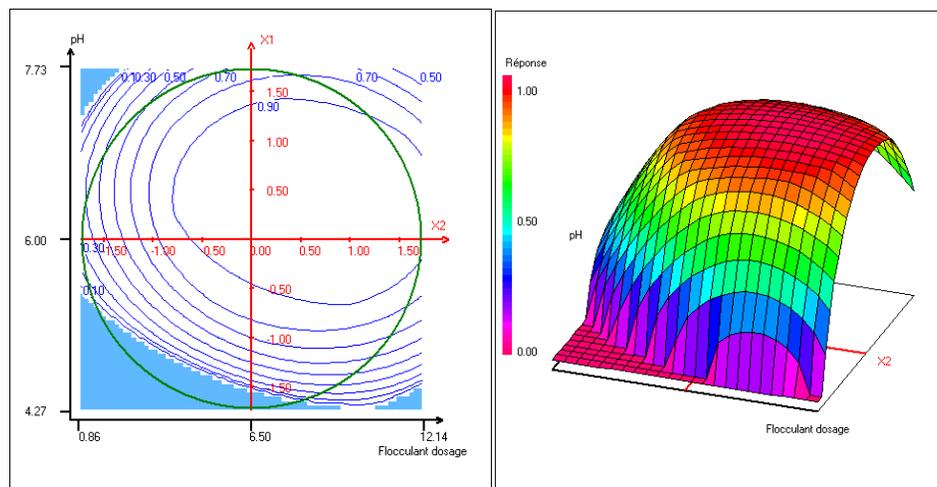


Figure 5. Variation of the desirability function for a multicriteria optimization. (1) plan: Coagulant dosage, Flocculant dosage, pH = 6.4; (2) plan: Coagulant dosage, pH, FACTEURS FIXES: Flocculant dosage = 8.6mg/L; (3) plan: Flocculant dosage, pH, FACTEURS FIXES: Coagulant dosage = 1267.3 mg/L.

The optimal conditions corresponding to the maximum value of the desirability function (99.17%) are (pH=6.4, flocculant dosage=8.6 mg/L and Coagulant dosage=1267.3 mg/L). The response values calculated from the model for these experimental conditions are given in **Table 8**.

Table 8. Confirmation experiments at optimum Coagulation/ flocculation conditions.

Response	Responses (removal, %)		
	COD	Oil & Grease	Turbidity
Experimental values	86	96	94
Calculated value	88	97	94
Calculated value	89.6	95.0	95.3

To approve the agreements of the results attained from the model and experiments. The values of responses are illustrated in **Table 8** and compared with the values calculated by the model. The deviation between the experiment and the predicted values is inferior to 2%, pointing out the good precision of the model. The results presented in **Table 8** confirmed that the experimental testing in the optimum conditions was in good agreement with RSM results.

CONCLUSIONS

The waste streams which come out of vegetable oil refinery without any treatment create environmental problem such as threat to aquatic life due to their high organic content. The treatment of wastewater laden with fatty oils has become a necessity in order to reduce pollution considerably. The physicochemical process by coagulation-flocculation appears to be very interesting for producing water that meets the quality standards of the water used for irrigation.

The present study concerns applying the experimental plan to determine the optimal conditions for the treatment of these discharges by coagulation flocculation to reduce pollution. RSM using CCD was applied to assess the effects of coagulant, flocculant, and pH doses on treatment efficiency to determine optimal coagulant and flocculant conditions subsequently. The results showed that the three factors considered in this study played an essential role in the removal efficiency of COD, turbidity and oil and grease. The optimal conditions obtained for the coagulant dose, the dose of flocculant, and the pH were 1267, 8.6 mg / L, and 6.4, respectively. Under these optimal conditions, about 90% of COD removal was obtained and 95% to reduce turbidity and oils and fats. The optimal conditions (concentration of coagulant and flocculant, pH) have shown that coagulation-flocculation constitutes an exciting element to evaluate the optimal concentrations for an efficient treatment of wastewater loaded with oils and fats.

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